# Simulating gliders

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in collaboration with

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### Outline

- Introduction
- 2 The models
- Results
- GTI compared with real glider data
- Conclusions





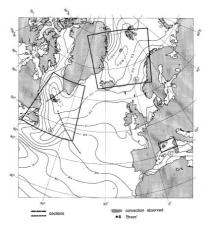
### Why simulating?

- No gliders out there yet,
- Examining observational capabilities,
- Evaluating sampling strategies.

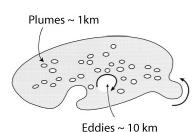




### Background



(Marshall & Schott, 1999)



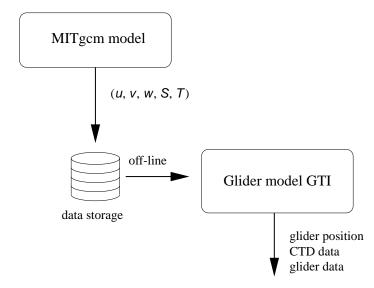
(Marshall & Schott, 1999)

Convective mixing





#### Model overview







# MITgcm model highlights

- non-hydrostatic,
- curvilinear grid,
- netcdf output,
- constant viscosity,
- freely available.

Web: http://mitgcm.org





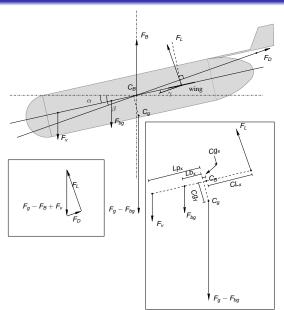
# GTI model highlights

- o considers all forces on glider,
- looks up in netcdf *u*, *v*, *w* using cubic interpolation,
- and T and S using tri-linear interpolation
- user prescribed waypoints, gliding angles etc.,
- freely available from our website,
- C-code.





# GTI model highlights







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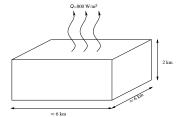
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Web: http://www.noc.soton.ac.uk/omf/lmm/glider



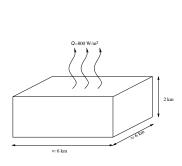


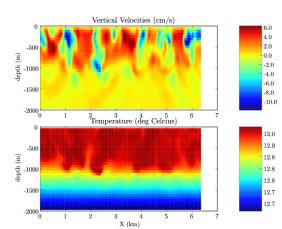
# Model setup





# Model setup

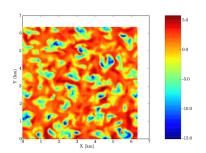


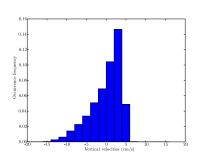






### **Plumes**

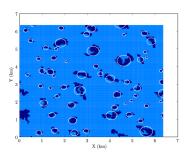


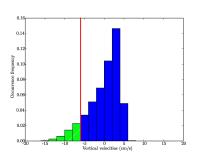






### **Plumes**

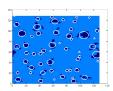








### Some numbers...



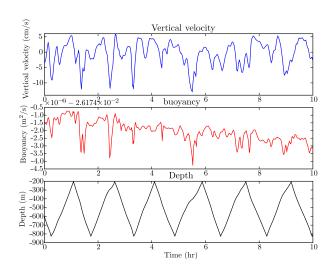
Plume density:	0.11	-
Average plume size:	pprox 300	m
Number of plumes:	59	-
Averaged distance between		
plumes:	pprox2	km

Can we measure these numbers from glider data?





#### Glider time series...

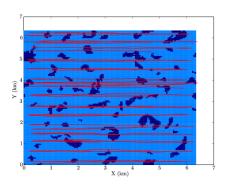






# Plume density

#### Using 15 gliders:



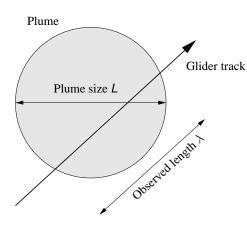
Plume density MITgcm: 0.11 Plume density GTI: 0.11

# plumes MITgcm: 59 # plumes GTI: 67





### Plume sizes

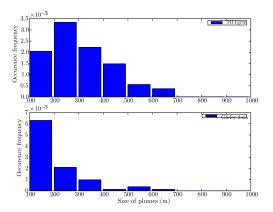


Expected value observed length:

$$E(\lambda) = \frac{\pi L}{4}$$



#### Plume sizes

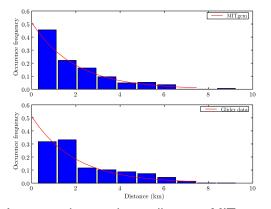


Average plume size MITgcm: 304 m Average observed plume size GTI: 212 m Average plume size GTI: 270 m





#### Plume-Plume distances



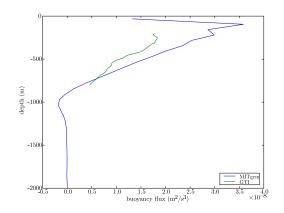
Average plume–plume distance MITgcm: 1.9 km Average plume–plume distance GTI: 2.3 km





## **Buoyancy fluxes**

### Buoyancy flux = $\overline{w'b'}$



- Need many data to compute averages
- Need high quality estimates of vertical water velocities





Vertical velocity of glider with respect to fixed reference frame:

$$w \approx \frac{1}{\rho g} \frac{\mathrm{d}P}{\mathrm{d}t}$$

which can be decomposed into:

$$W = W_{\text{glider}} + W_{\text{ambient water}}$$

What is  $w_{glider}$ ?





### Vertical velocity estimate

Vertical velocity of glider with respect to fixed reference frame:

$$w \approx \frac{1}{\rho g} \frac{\mathrm{d}P}{\mathrm{d}t}$$

which can be decomposed into:

$$W = W_{\text{glider}} + W_{\text{ambient water}}$$

What is  $w_{\text{alider}}$ ?

Optimally tuned glider dynamics model yields best estimate for vertical veloctly from pressure fluctuations.



# Tuning the GTI model

Comparing real glider data (*Bellamite* Mallorca trials April 2006) with GTI model:

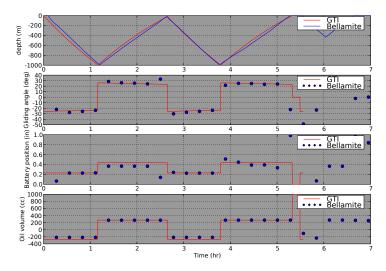
#### Tuning paramters (short list):

- mass
- volume
- drag coefficients
- centre of mass(es)
- battery pack position
- ...





#### Data from GTI model and a mission from Bellamite







### Conclusions

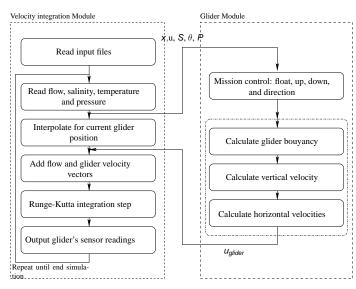
#### GTI:

- Research tool
  - What to expect from glider data when flown in a convective area?
  - Evaluating sampling strategies.
- Tuning glider's dynamic model
  - Allows accurate as possible vertical flow velocity estimates.





#### GTI model overview

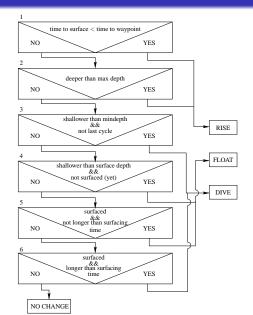






### GTI mission control

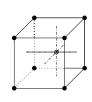
Introduction

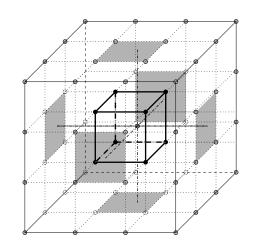






### MITgcm data interpolation









Extra

#### The vertical and horizontal components of the force balance:

$$F_g - F_B + F_V - \cos \beta F_L - \sin \beta F_D = 0$$
$$\cos \beta F_D - \sin \beta D_L = 0$$

The lift force (thin plate-shaped wings):

$$F_L = \pi \gamma \rho A_W U^2$$

The drag force  $F_D$ 

$$F_D = \frac{1}{2} C_{dg} \rho A_g U^2$$

Torque balance:

$$\begin{split} \cos\alpha(\textit{F}_{\textit{g}} - \textit{F}_{\textit{bg}})\textit{Cg}_{\textit{x}} + \cos\alpha\textit{F}_{\textit{y}}\textit{Lp}_{\textit{x}} + \cos\alpha\textit{F}_{\textit{bg}}\textit{Lb}_{\textit{x}} \\ - \sin\alpha\textit{F}_{\textit{g}}\textit{Cg}_{\textit{y}} + \cos\gamma\textit{F}_{\textit{L}}\textit{C}_{\textit{Lx}} = 0. \end{split}$$





### The equations...

$$\gamma = \frac{C_{dg}A_g}{2\pi A_w \tan(\alpha + \gamma)}$$

$$\tan \alpha = \frac{(F_g - F_{gb})Cg_x + \cos^2 \gamma C_{Lx}(F_g - F_B + F_v) + Lb_x F_{gb} + Lp_x F_v}{(F_g - F_{gb})Cg_y + \cos \gamma \sin \gamma C_{Lx}(F_g - F_B + F_v)}$$

- $\mathbf{0}$  set  $\gamma = \mathbf{0}$
- 2 calculate  $\alpha$
- $\odot$  calculate  $\gamma$
- 1 loop back to 2, unless converged.



